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SHALLOW METALLIC S-SEAL

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SHALLOW METALLIC S-SEAL

BACKGROUND OF THE INVENTION

1. Field of the Invention

This invention generally relates to a metallic seal for creating a seal between a pair of members. More specifically, the present invention relates to a seal that provides a highly reliable seal by concentrating the available load over a narrow band (small sealing area equaling high contact stress) to produce a high quality sealing dam over a sufficient width to minimize leakage on a molecular level.

2. Background Information

A typical static seal assembly has a first member with a first mating surface, an annular seal of suitable sealing material (e.g., metal O-ring), and a second member with a second mating surface. A mechanical load is applied to the seal through the first and second mating surfaces of the members. Typically, the mechanical load is created by torquing down a multitude of fasteners such that a displacement, also known as compression, occurs between the sealing surfaces. The net loading of the contact surfaces creates the two sealing dams.

The low leakage requirement can be achieved by compressing a solid metal ring of rectangular cross-section with a sufficient force. One problem with a solid metal ring is that the force created could be of sufficient magnitude to cause plastic deformation of the mating surfaces of the members. This plastic deformation of the mating surface is called brinelling. Once brinelled, the probability of proper re-sealing is drastically reduced without first repairing the damaged sealing surfaces.

The design requirements for static sealing therefore requires an optimum load level and flexibility. A good static seal when compressed must be able to generate load levels large enough to seal, but not large enough to brinell the cavity surfaces. Currently, there are many types of metallic seals in the prior art.

The metallic "O" rings were an early effort to meet these conflicting design requirements. However, the resiliency of this type of seal is rather limited because the "O" ring, whether solid or hollow, is usually too stiff, and is inherently expensive. The development of the C-shaped seal was an improvement to the "O" ring. In particular, by simply discarding a portion of the "O", the hoop restraint of the seal is greatly reduced and the seal becomes more flexible. However, the basic "C" seals typically cannot reach the desirable standard vacuum level of 1×10^{-9} cc/sec He

leakage rate or better without modification and without being coated with very soft plating materials. Some previous C-shaped seals have been designed to provide this level of seal integrity.

5 In addition to typical "C" seals, other prior seals include spring-energized "C" seals, spring-energized "C" seals with triangular feature (Delta-seal), deformable metallic gaskets, E-seals with single or multiple convolutions. Some of these previous designs can provide the level of seal integrity provided by the disclosed device at comparable load levels or physical restraints.

10 Examples of these prior sealing rings are disclosed in U.S. Patent No. 4,813,692 and U.S. Patent No. 4,854,600. However, the seals of these two patent address semi-dynamic applications where the two sealing surfaces are moving relative to each other. These patents are associated with larger cross sections and the method of deformation uses both axial bending and torsion.

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In view of the above, it will be apparent to those skilled in the art that there exists a need for improved metallic sealing rings with optimized sealing areas that can be use at high temperatures and pressures while providing high reliability and pressure tight sealing. This invention addresses this need in the art as well as other needs, which will become apparent to those skilled in the art once given this disclosure.

20 SUMMARY OF THE INVENTION

One object of the present invention is to provide a highly reliable metallic seal that is relatively inexpensive to manufacture.

25 Another object of the present invention is to provide a metallic seal, which has geometrically simple cross sections, and can be manufactured with existing equipment in large quantities with tight tolerances.

Still another object of the present invention is to provide a highly reliable metallic seal, which concentrates the available load over a narrow band which minimizes the required load to compress the seal by optimizing the sealing dam width.

30 Yet another object of the present invention is to provide a metallic seal in which the seal dam does not significantly shift during compression of the seal.

Another object of the present invention is to provide a metallic seal which has a leakage rate of less than 1×10^{-9} cc/sec He leakage rate or better.

The foregoing objects can basically be attained by providing a metallic seal that concentrates the available load over a narrow band to produce a sealing dam over a sufficient width to minimize leakage while optimizing the load required to compress the seal. The metallic seal comprises a first annular end section, a second annular end section and an annular center section. The first annular end section has a first annular sealing surface facing in a first direction and lying in a first plane to contact a first member for creating a first annular sealing dam therebetween. The second annular end section has a second annular sealing surface facing in a second direction that is opposite to the first axial direction, and lying in a second plane that is substantially parallel to the first plane to contact a second member for creating a second annular sealing dam therebetween. The annular center section extends between the first and second annular end sections to form a ring having a central passageway with a center longitudinal axis. The third annular section is frustoconical tube with the first and second annular end sections being contiguously arranged at opposite ends of the annular center section such that sealing loads applied substantially perpendicularly on the first and second annular sealing surfaces primarily deform due to torsional stress of the metallic seal.

These and other objects, features, aspects and advantages of the present invention will become apparent to those skilled in the art from the following detailed description, which, taken in conjunction with the annexed drawings, discloses a preferred embodiment of the present invention.

BRIEF DESCRIPTION OF THE DRAWINGS

Referring now to the attached drawings which form a part of this original disclosure:

Figure 1 is a side elevational view of a shallow metallic seal in accordance with a first embodiment of the present invention, with the thickness of the seal exaggerated for purposes of illustration;

Figure 2 is a top plan view of the shallow metallic seal illustrated in Figure 1;

Figure 3 is a cross-sectional view of the shallow metallic seal illustrated in Figures 1 and 2, as seen along section line 3-3 of Figure 2;

Figure 4 is an enlarged cross-sectional profile of the shallow metallic seal illustrated in Figures 1-3 prior to compression of the metallic seal, i.e., unloaded;;

Figure 5 is an exploded, longitudinal cross-sectional view of the shallow metallic seal illustrated in Figures 1-4 together with a seal assembly having a pair of mating members which are coupled together by fasteners to axially compress the metallic seal for creating an annular seal therebetween;

Figure 6 is a longitudinal cross-sectional view, similar to Figure 5, of the mating members and the metallic seal, but after the mating members have been coupled together by the fasteners to compress the metallic seal for creating an annular seal therebetween; and

Figure 7 is a longitudinal cross-sectional view of a shallow metallic seal according to a second embodiment of the present invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Initially referring to Figures 1-4, a shallow metallic seal 10 in accordance with a first embodiment of the present invention is illustrated. The shallow metallic seal 10 is illustrated as being circular. However, it will be apparent to those skilled in the art from this disclosure that the shallow metallic seal 10 could have other types of non-circular ring shapes and can also be produced in a variety of heights. Moreover, the thickness of the metallic seal 10 in the attached drawings has been exaggerated for purposes of illustration.

The purpose of the metallic seal 10 is to provide a seal between two opposing members, e.g., either metal to metal, metal to ceramic, ceramic to ceramic, or any appropriate combination of materials commonly used in critical fluid and/or gas sealing. Additionally, the metallic seal 10 can be used between flanges or components for any fluid control or pneumatic application. The metallic seal 10 will most typically be used in a groove, counterbore or between relatively flat surfaces providing a fixed separation of the components to be sealed. The metallic seal 10 can be produced in circular or non-circular configurations and may also be produced in a variety of heights.

As explained below in more detail, the shallow metallic seal 10 of the present invention provides highly reliable sealing between two members by concentrating the available load over a narrow band (small surface area equaling high contact stress).

These narrow sealing bands or surfaces produce a high quality sealing dam over a sufficient width to minimize leakage on a molecular level. By minimizing the seal dam widths over which the intimate contact between seal and mating surfaces is needed, a high performance seal can be achieved without high compression loads. In other

words, the shallow metallic seal 10 of the present invention allows its substantially parallel surfaces of the seal 10 to be in intimate contact with the two cavity faces, resulting in a controlled contact stress (load divided by the area of the annulus).

5 The shallow metallic seal 10 of the present invention is designed to be used in to a wide range of sealing performance. The shallow metallic seal 10 of the present invention is especially applicable to the semiconductor equipment industry, the vacuum equipment industry, the data storage device industry, or any other industry where high reliability and/or extremely tight sealing (1×10^{-9} cc/sec He leakage rate or better) is required. The shallow metallic seal 10 of the present invention is also applicable
10 anywhere that the basic configuration lends itself to the sealing gland dimensions or the available bolt loading. For example, the shallow metallic seal 10 can be used in a wide variety of applications required in the Ultra High Vacuum (UHV) industry, the Aerospace, the Power Generation industry and any other industry that requires the above stated functionality.

15 In particular, the shallow metallic seal 10 provides high pressure, high temperature sealing with rates of .01 SCFM per inch of diameter to high reliability and pressure tight with rates less than 1×10^{-9} cc / sec. The shallow metallic seal 10 of the present invention is designed to perform at wide range of force to compression or pounds per circumferential inch (PCI).

20 The shallow metallic seal 10 has a uniform cross sectional profile as seen in Figure 4. The term "cross-sectional profile" as used herein and in the claims refers to a partial cross sectional shape of a portion of an annular seal as defined by a longitudinal plane passing through only one point of the annular seal.

The shallow metallic seal 10 is constructed of a ductile alloy that is pressed
25 worked to form an annular member that has a cross sectional profile as seen in Figure 4. For example, the base material of the seal 10 is constructed of a ductile alloy or metallic element such as tin, nickel, aluminum, copper, stainless steel, Inconel and other nickel based alloys that improve seal integrity. Preferably, the base material of the seal 10 is formed of a corrosion resistant alloy that is selected from the group of
30 nickel based alloys, copper based alloys, tin, aluminum based alloys and stainless steel. Optionally, a softer ductile coating could also be employed over the base material (ductile alloy). Examples of such ductile coatings include, but not limited to, tin, aluminum, nickel indium, silver, PFA, PTFE, etc. The ductile coating preferably has a

thickness between about 0.001 inch and 0.006 inch. This ductile coating can cover the entire seal surfaces or can be located only at the sealing surfaces. Other metal elements and non-metallic compounds can be employed as well for the coating.

5 The shallow metallic seal 10 allows for seal cavity tolerances by designing the seal stiffness to be acceptable over the combined tolerance range of the cavity plus the seal. By designing the seal's cross-sectional profile as shown in Figure 4, the deflection of the section is controlled. By varying the cross section (thickness, radius of curvature at the seal interface, angle, height and radial width) the load can be designed such that the seal will function in a variety of seal gland depths, and with different coatings, each
10 with their own specific yield strengths, i.e. requiring more or less load to create a condition whereby the coating plastically deforms over a given width.

As seen in Figures 5 and 6, a sealing assembly 12 in accordance with a first embodiment of the present invention is diagrammatically illustrated to show the metallic seal 10 being used. More specifically, the seal assembly 12 includes a first
15 member 14, with a first mating or contact surface 16 and a second member 18 having a second mating or contact surface 20 for contacting the seal 10. The first and second members 14 and 18 are coupled together by a plurality of fasteners or bolts 22. The first and second members 14 and 18 can be any two members or devices that need a seal there between. Thus, the first and second members 14 and 18 are not illustrated
20 with any particular structure.

For example, a variant of the metallic seal 10 can be constructed such that an effective, low cost seal can be achieved for high temperature and/or high pressure pneumatic applications. This variant can be constructed in a similar manner as the high leak integrity version illustrated herewith.

25 The shallow metallic seal 10 is a one-piece, unitary member formed from a single sheet material. Optionally, the metallic seal 10 can have a soft coating overlying the base material. Basically, the cross-sectional profile of the shallow metallic seal 10 can be divided into three annular sections three annular section, i.e., a first annular end section 31, a second annular end section 32 and a third annular center
30 section 33. In the illustrated embodiment, the first and second annular end sections 31 and 32 have curved cross-sectional profiles, while the third annular center section 33 has a straight cross-sectional profile. Thus, the annular sections 31-33 are configured to form a somewhat S-shaped cross section. This S-shaped cross section is preferably

uniform along the entire circumference of the metallic seal 10. In the illustrated embodiment, the third annular center section 33 is a frustoconical section. However, the third annular center section 33 can have a curved cross-sectional profile and be a non-circular section viewed in the axial direction. In any event, the third annular center section 33 is frustoconically shaped. The term " frustoconically shaped " as used herein and in the claims refers to an annular section having first and second annular ends with one of the ends having a diameter or transverse dimension that is larger than the diameter or transverse dimension of the other end and the annular section between the first and second annular ends be non-undulated.

The first annular end section 31 has a first annular sealing surface 34 facing in a first axial direction A_1 and lying in a first flat contact plane P_1 . The first annular sealing surface 34 contacts the first contact surface 16 of the first member 14 for creating a first annular sealing dam D_1 therebetween. The second annular end section 32 has a second annular sealing surface 36 facing in a second axial direction A_2 that is opposite to the first axial direction A_1 , and lies in a second flat contact plane P_2 that is substantially parallel to the first flat contact plane P_1 . The second annular sealing surface 36 contacts the second contact surface 20 of the second member 18 for creating a second annular sealing dam D_2 therebetween. The annular center section 33 extends between the first and second annular end sections 31 and 32 to form a ring having a central passageway 38 with a center longitudinal axis C.

The first and second sealing surfaces 34 and 36 are preferably convexly curved surfaces with identical curvatures that extend through an arc of about 60° . In other words, the first and second sealing surfaces 34 and 36 are basically annular sealing lines S_1 and S_2 with no radial width prior to compression of the seal 10. By tightening the fasteners 22, the metallic seal 10 is loaded, and thus, compressed to plastically deform the seal primarily through torsion and create the pair of annular seal dams D_1 and D_2 between the metallic seal 10 and the first and second members 14 and 18. Deformation of the metallic seal 10 is about 10% to 25% of the axial height of the seal 10 between its sealing surfaces 34 and 36. Once the seal 10 is compressed, the first and second sealing surfaces 34 and 36 are deformed to form flat sealing surfaces that correspond to the first and second annular sealing dams D_1 and D_2 . The minimum effective widths of first and second annular sealing dams D_1 and

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D₂ of the first and second sealing surfaces 34 and 36 lies within the range of about 0.005 inch to about 0.040 inch.

5 The first and second sealing surfaces 34 and 36 are spaced apart by a first distance or height d₁ measured parallel to the center longitudinal axis C that is smaller than a second distance (d₂) measured perpendicular to the center longitudinal axis C between the first and second sealing surfaces 34 and 36. In the illustrated embodiment, the first distance d₁ is substantially equal to a second distance d₂.

10 The third annular section 33 is a frustoconical tube. The first and second annular end sections 31 and 32 are contiguously arranged at opposite axial ends of the annular center section 33 such that sealing loads applied substantially perpendicularly on the first and second annular sealing surfaces 34 and 36 primarily deform due to torsional stress of the metallic seal 10. In other words, the metallic seal 10 is deformed less than 50% by collapsing or axial bending such as in the S-shaped seals disclosed in U.S. Patent Nos. 4,813,692 and 4,854,600. Preferably, the metallic seal 10 only
15 collapses or bends axially by about 20%. The annular center section 33 preferably slopes about 45° relative to the first and second planes P₁ and P₂.

20 The geometric and dimensional characteristics of seal 10 can be particularly seen in Figure 4. Referring initially to Figure 2, the outer diameter of seal 10 can be any desired shape depending upon the application of seal 10, i.e., there is no limit to its outer diameter. The inner diameter of seal 10 should be at least about 0.150 inch or greater. The free axial height d₁ of seal 10 is typically between about 0.030 inch to about 0.250 inch. In one example of the seal 10, the height d₁ is 0.035 inch, the outer diameter is 0.315 inch, and the inner diameter is 0.245 inch.

25 In this embodiment, the first and second directions A₁ and A₂ of the first and second sealing surfaces 34 and 36 face in directions that are substantially parallel to the center longitudinal axis C. Alternatively, as seen in Figure 7, a seal 110 is illustrated having the first and second sealing surfaces 134 and 136 facing substantially perpendicular to the center longitudinal axis C. In other words, the first and second sealing surfaces 134 and 136 are concentric sealing surfaces that face
30 either towards or away from the center longitudinal axis C. The metallic seal 110 is nearly identical to seal 10, discussed above, except that for the cross section as been rotated. In view of the similarities between seal 110 and seal 10, discussed above, seal 110 will not be discussed or illustrated in detail herein. Basically, the metallic

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seal 110 has a first annular end section 131, a second annular end section 132 and an annular center section 133.

Although only a portion of metallic seal 110 is illustrated herein, it will be apparent to those skilled in the art from this disclosure that seal 110 is a continuous ring which can be either circular or non-circular. Preferably, the cross-section of the seal 110 is uniform.

The terms of degree such as "substantially", "about" and "approximately" as used herein mean a reasonable amount of deviation of the modified term such that the end result is not significantly changed. These terms should be construed as including a deviation of at least $\pm 5\%$ of the modified term if this deviation would not negate the meaning of the word it modifies.

While only selected embodiments have been chosen to illustrate the present invention, it will be apparent to those skilled in the art from this disclosure that various changes and modifications can be made herein without departing from the scope of the invention as defined in the appended claims. Possible variations of the illustrated the seal 10 include a range of diameters, shapes, heights, coatings, base materials chosen for coefficient of thermal expansion matches, pressure or vacuum sealing, sealing any fluid by choosing compatible materials, or any other variation typically used to configure the seal 10 for a given application. Another advantage of the cross section is the ability to seal on the inner and outer diameters and may be extended to other uses and industries. Furthermore, the foregoing description of the embodiments according to the present invention are provided for illustration only, and not for the purpose of limiting the invention as defined by the appended claims and their equivalents.